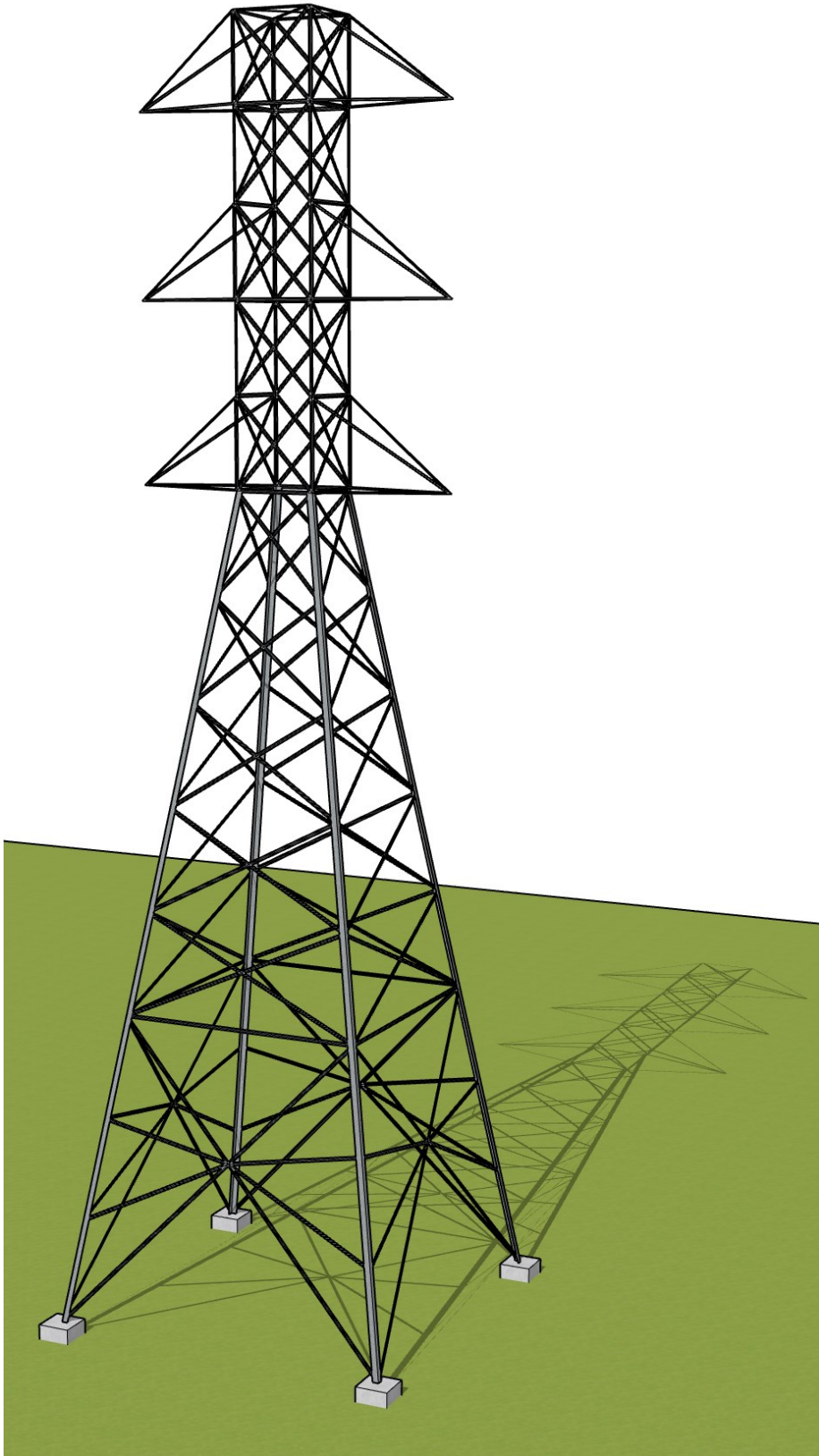
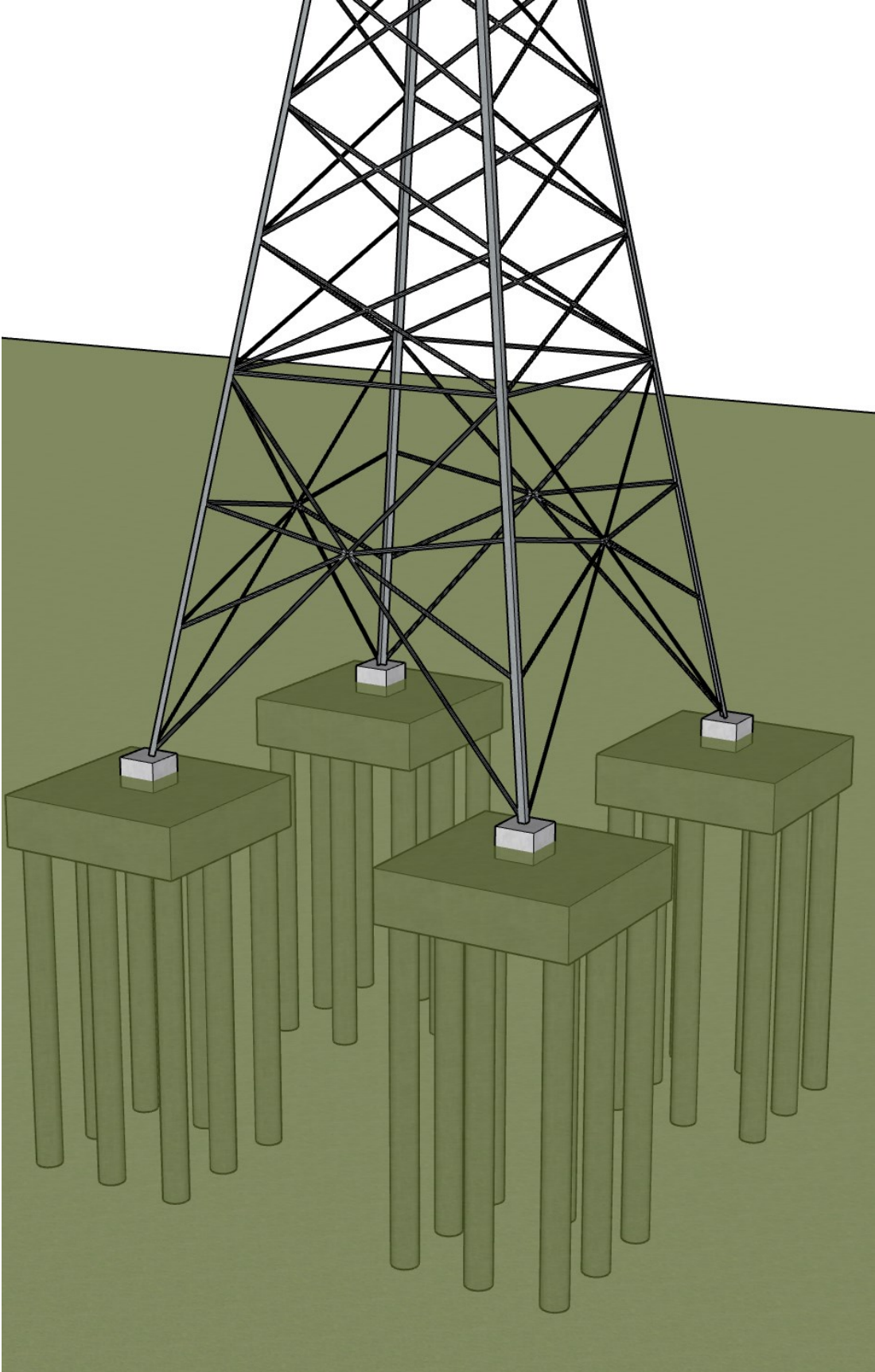


Transmission Tower Reinforced Concrete Pile Cap Foundation





Transmission Tower Reinforced Concrete Pile Cap Foundation

The purpose of a transmission line tower is to support conductors carrying electrical power and one or two ground wires at suitable distances above the ground level and from each other. The transmission line towers cost about 35 to 45 per cent of the total cost of the transmission line. A transmission tower is commonly a space truss and is an indeterminate 3D structure. This case study focuses on the design of transmission tower foundation using the engineering software program [spMats](#). The tower under study is a galvanized steel tower type 2DT6 for 230kV transmission line with a total height of 100 ft. All the information provided by the structural engineer regarding the transmission tower are shown in the following figures and design data section and will serve as input for foundation design. Because of tower height, significant uplift is expected and a pile supported foundation is selected to resist the design overturning moments. Eight 24" diameter piles are assembled in a pile cap as shown in the following figure.

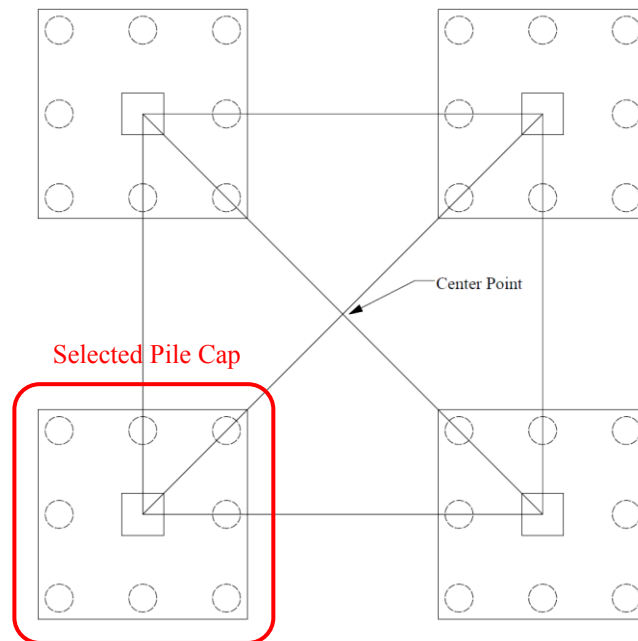


Figure 1 – Transmission Tower Foundation Layout Plan

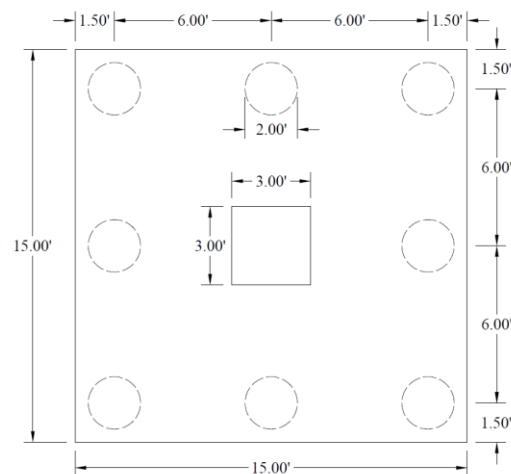


Figure 2 – Transmission Tower Foundation Geometry

Code

Building Code Requirements for Structural Concrete (ACI 318-14) and Commentary (ACI 318R-14)

Reference

spMats Engineering Software Program Manual v8.50, StructurePoint LLC., 2016

Design Data

Concrete Pier

Size = 3 ft x 3 ft

Height = 2.3 ft

Weight = 3 kips

Clear Cover = 2 in.

Pile Cap Foundation

$f_c' = 3,000$ psi

$f_y = 60,000$ psi

Thickness = 4 ft

Clear Cover = 2 in.

Pile Cap Weight = 133.7 kips

Superimposed Soil Weight = 24.1 kips = 115 psf over the foundation (pile cap) cross-section

Concrete Piles

$f_c' = 4,000$ psi

$f_y = 60,000$ psi

Diameter = 2 ft

Clear Cover = 3 in.

Length = 26 ft

Center-to-Center Distance = 6 ft

Number of Piles Per Leg = 8 Piles

Pile embedment = 6 in.

Foundation Loads

$F_z = 937.0$ kips

$M_y = 610$ kips-ft (Reversible)

$M_x = 568$ kips-ft (Reversible)

Contents

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3. Pile Reactions	7
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1. Foundation Analysis and Design – spMats Software

[spMats](#) uses the Finite Element Method for the structural modeling, analysis and design of reinforced concrete slab systems or mat foundations subject to static loading conditions.

The slab, mat, or footing is idealized as a mesh of rectangular elements interconnected at the corner nodes. The same mesh applies to the underlying soil with the soil stiffness concentrated at the nodes. Slabs of irregular geometry can be idealized to conform to geometry with rectangular boundaries. Even though slab and soil properties can vary between elements, they are assumed uniform within each element. Piles are modeled as springs connected to the nodes of the finite element model. Unlike for springs, however, punching shear check is performed around piles.

For illustration and purposes, the following figures provide a sample of the input modules and results obtained from an spMats model created for the transmission tower reinforced concrete foundation (pile cap) in this example.

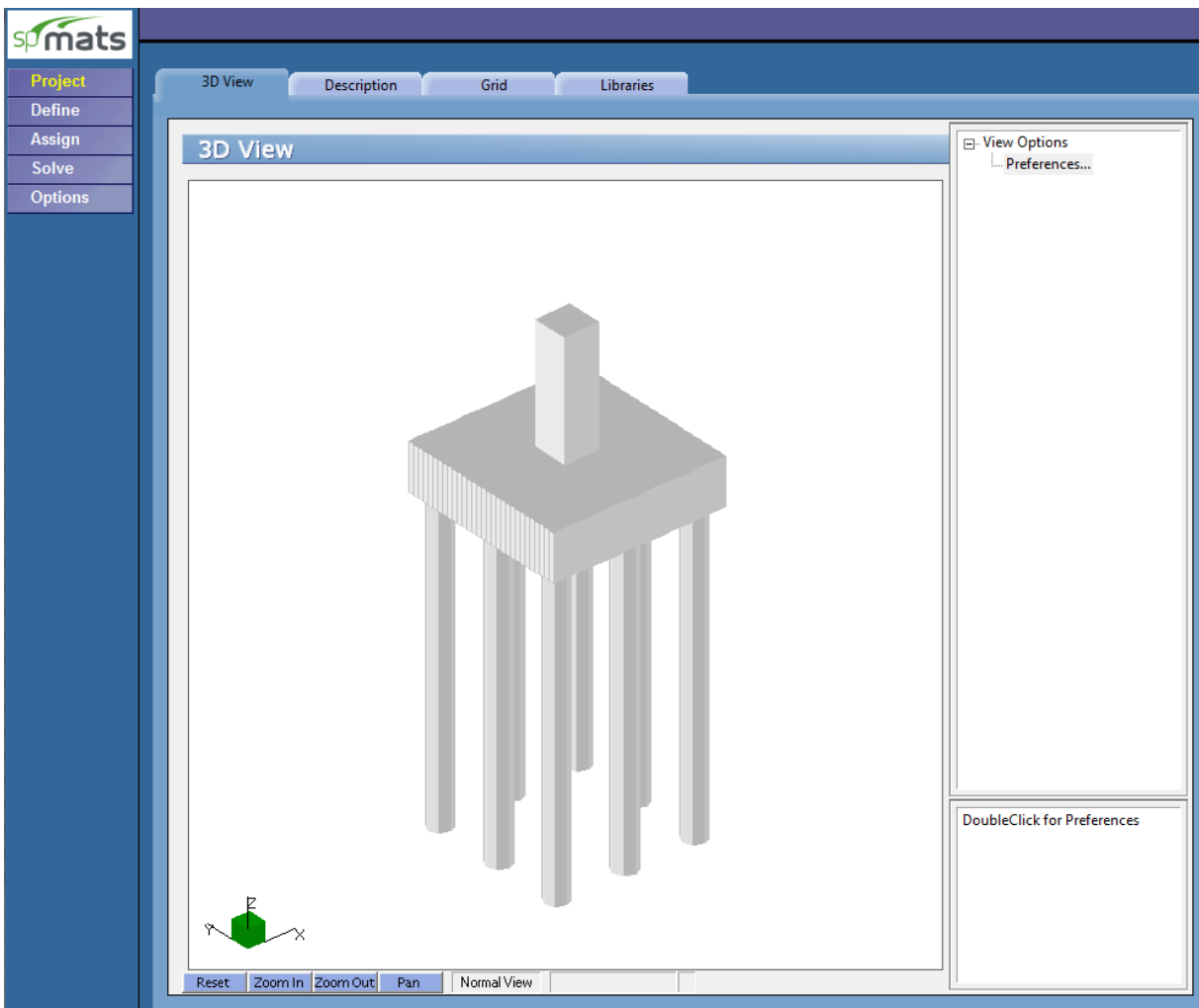


Figure 3 – Transmission Tower Foundation (Pile Cap) Model – 3D View

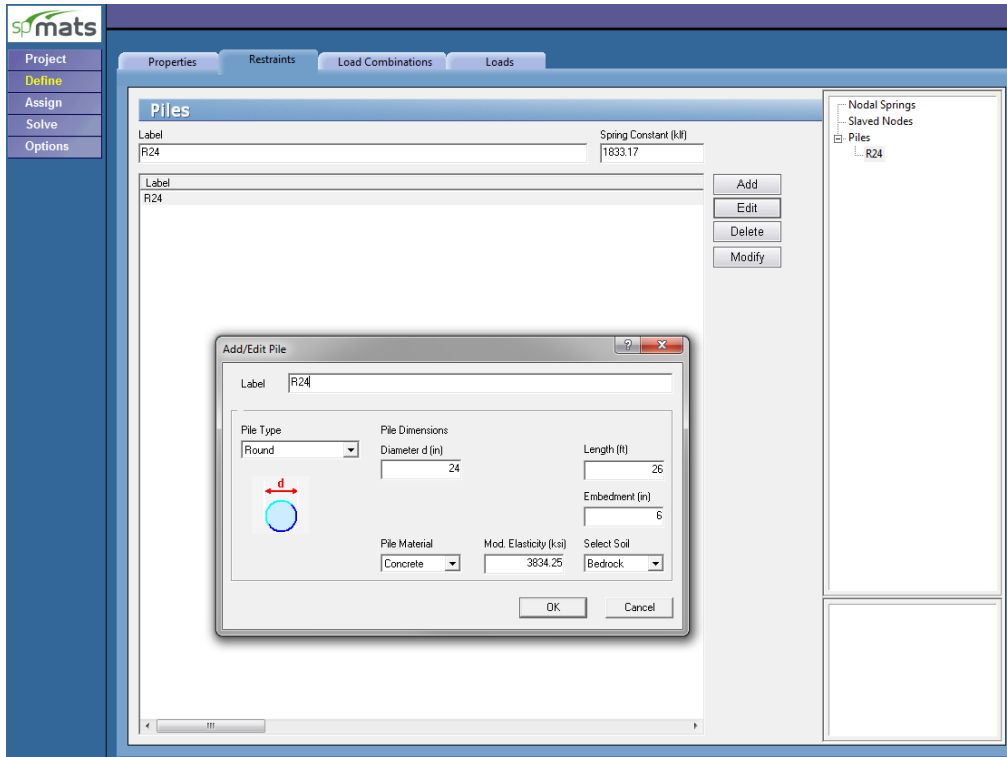


Figure 4 –Defining Piles

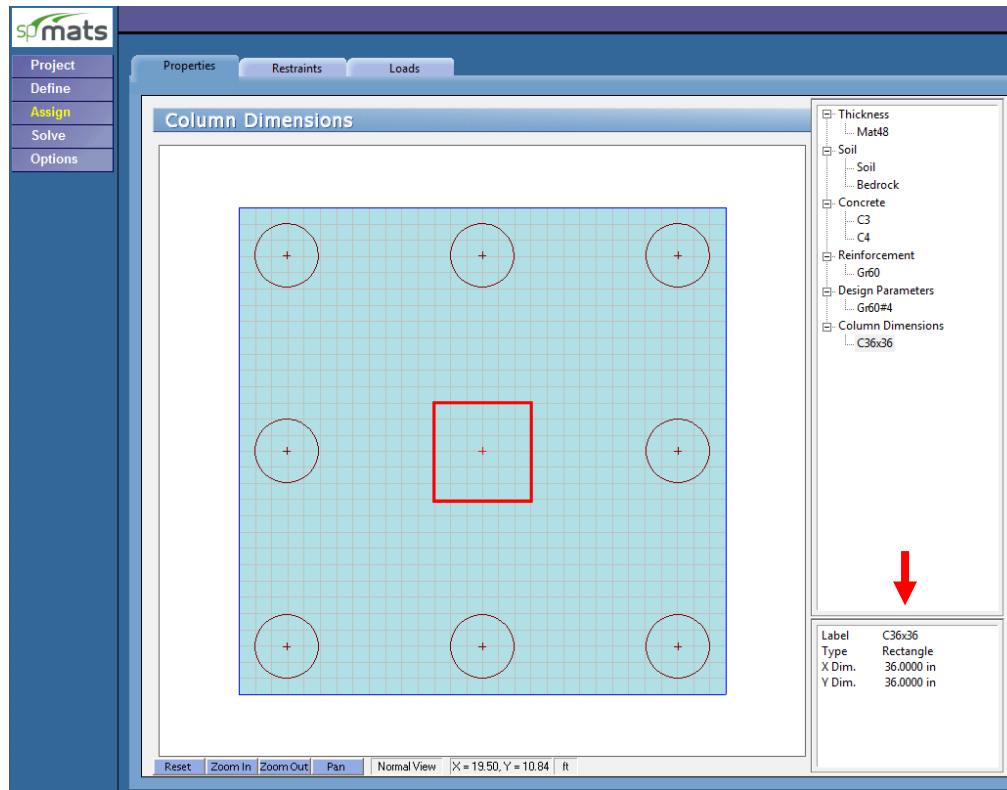


Figure 5 – Assigning Concrete Pier

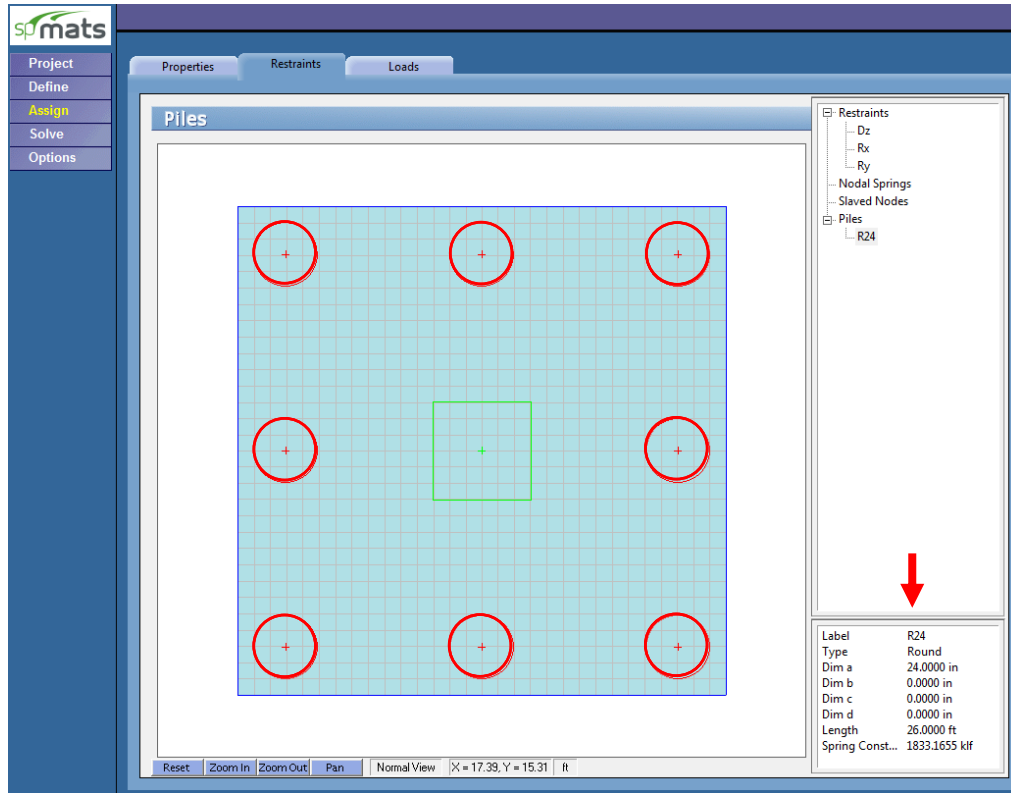


Figure 6 – Assigning Piles

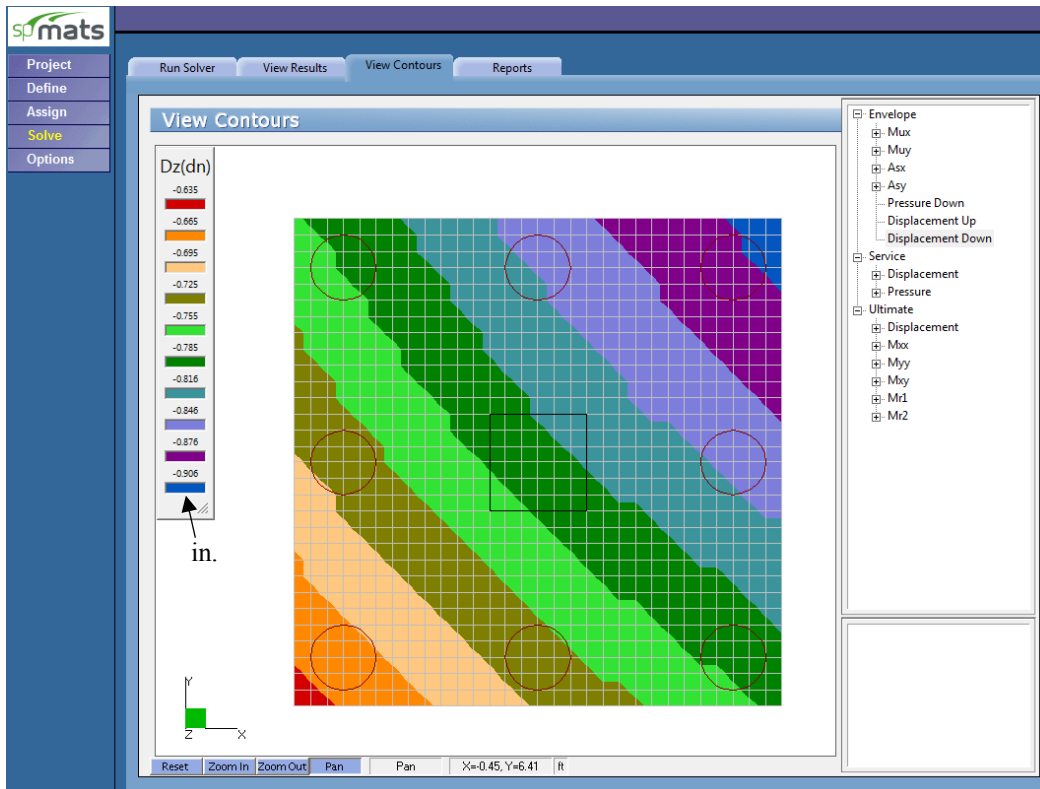


Figure 7 – Transmission Tower Foundation (Pile Cap) Vertical Displacement Contour

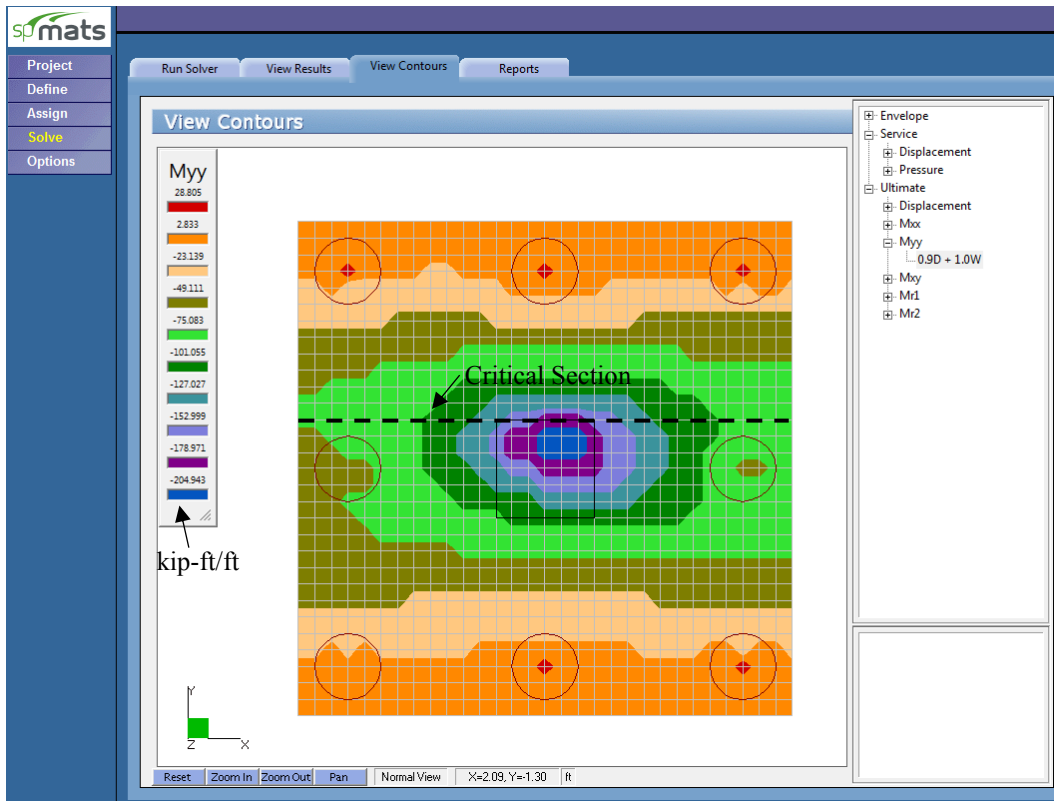


Figure 8 – Transmission Tower Foundation (Pile Cap) Moment Contour along Y-Axis

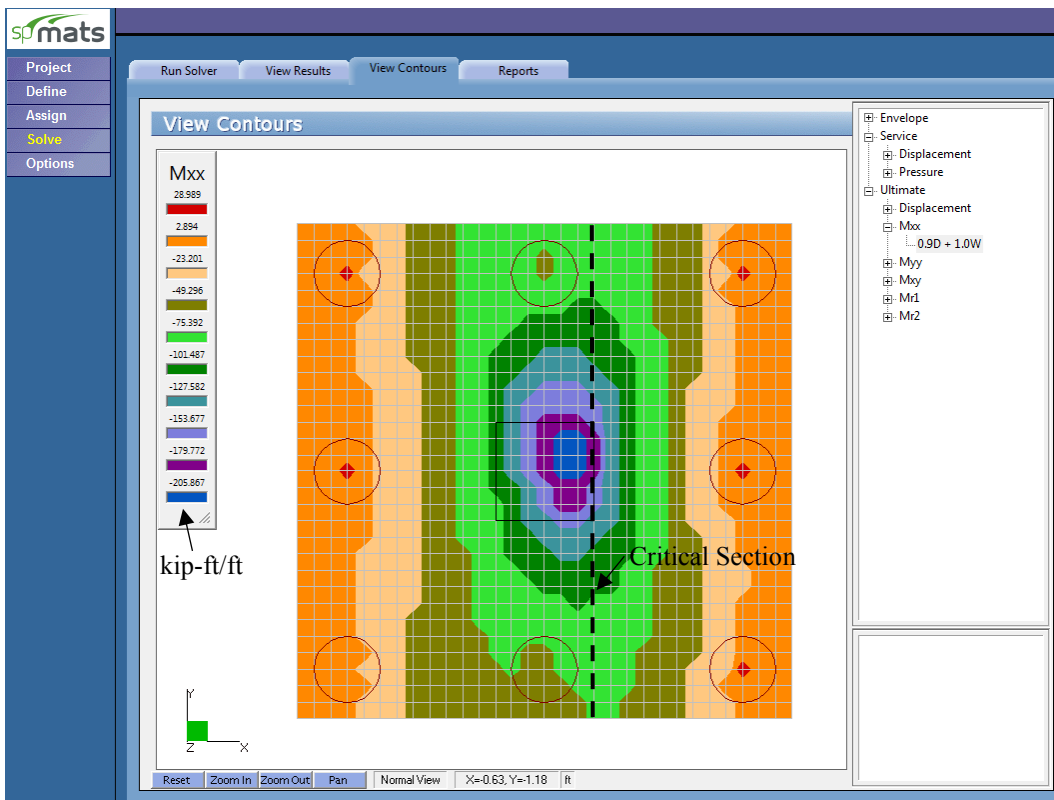


Figure 9 – Transmission Tower Foundation (Pile Cap) Moment Contour along X-Axis - Complete Model

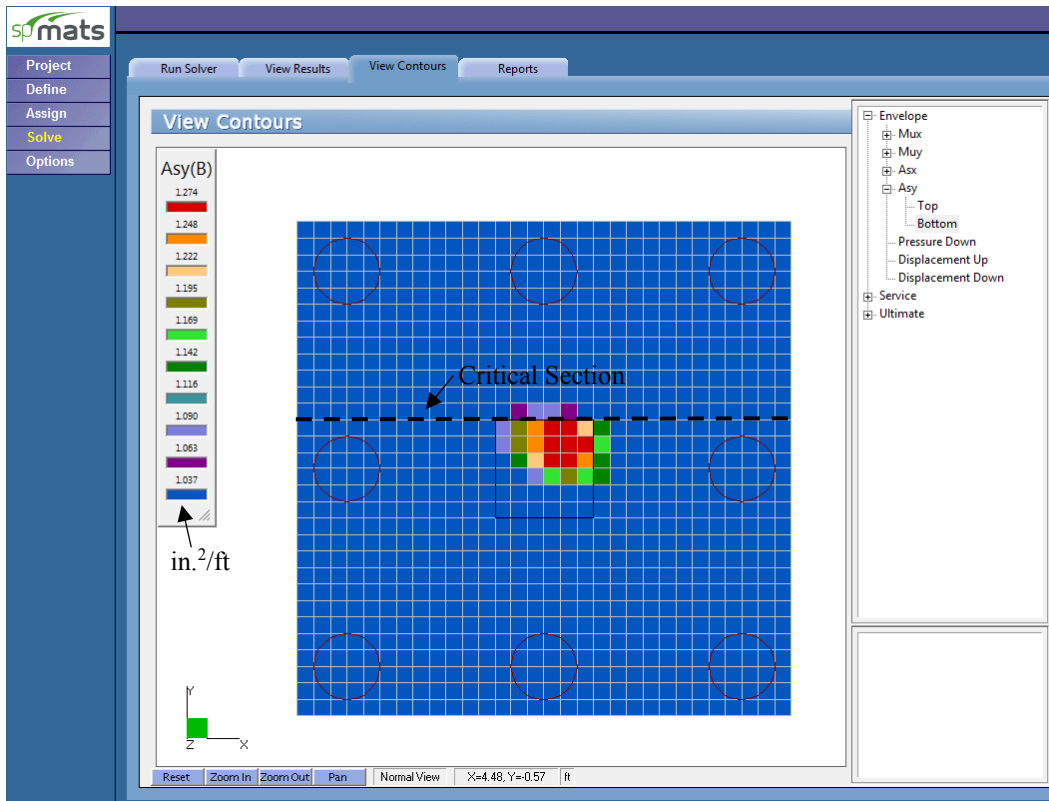


Figure 10 – Required Reinforcement Contour along Y Direction

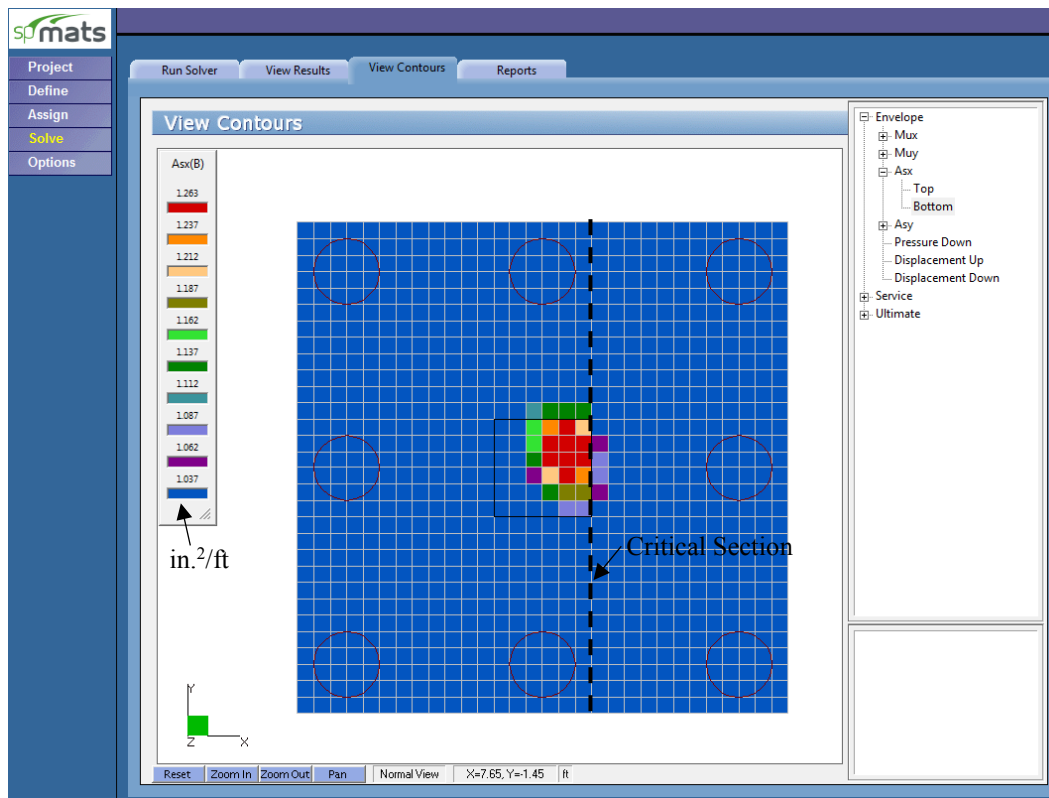


Figure 11 – Required Reinforcement Contour along X Direction

2. Two-Way Punching Shear Check - Piles

According to ACI 312-14 (R13.2.7.2), if shear perimeters overlap, the modified critical perimeter should be taken as that portion of the smallest envelope of individual shear perimeters that will actually resist the critical shear for group under consideration. [spMats](#) reports standard shear perimeter for three conditions (interior, edge, and corner) only considering adequate spacing and edge distance is provided to prevent overlapping or truncated shear perimeter.

```

B7 - Punching Shear Around Piles (Ultimate Load Combinations):
=====
Units --> Applied Shear Force Vu (kips), Applied Moments Mux, Muy (k-ft)
          Factored Shear Stress vu (psi), Factored Shear Resistance vc (psi)
          Concrete Strength f'c (psi), distances X_Offset, Y_Offset (ft)
          Average depth (in), Dimensions Bx, By (ft)
          Area (in^2), Jxx, Jyy, Jxy (in^4)
=====
Geometry of Resisting Area
-----
Node   Pile Label   Location   Average Depth   Dimensions Bx By   Centroid X_Offset Y_Offset
-----
97 R24   Inner         38.75     5.23  5.23   0.00  0.00
109 R24  Inner         38.75     5.23  5.23  -0.00  0.00
121 R24  Inner         38.75     5.23  5.23  -0.00  0.00
469 R24  Inner         38.75     5.23  5.23   0.00 -0.00
493 R24  Inner         38.75     5.23  5.23  -0.00 -0.00
841 R24  Inner         38.75     5.23  5.23   0.00 -0.00
853 R24  Inner         38.75     5.23  5.23  -0.00 -0.00
865 R24  Inner         38.75     5.23  5.23  -0.00 -0.00
-----
Properties of Resisting Area
-----
Node Pile Label   Area   Jxx   Jyy   Jxy
-----
97 R24   7631.13  4218034.00  4218033.50  -0.00
109 R24  7631.13  4218034.00  4218033.50   0.00
121 R24  7631.13  4218033.00  4218033.00  -0.00
469 R24  7631.13  4218034.00  4218033.50   0.00
493 R24  7631.13  4218033.00  4218032.50   0.00
841 R24  7631.13  4218033.50  4218033.00   0.00
853 R24  7631.13  4218033.50  4218033.00  -0.00
865 R24  7631.13  4218032.50  4218032.50  -0.00
-----
Ultimate Load Combination: 0.9D + 1.0W
-----
Factored Applied Forces:
-----
Node Pile Label   Vu   Mux   Gamma_X   Muy   Gamma_Y
-----
97 R24   79.96   -0.0  0.400   0.0  0.400
109 R24  94.44   -0.0  0.400  -0.0  0.400
121 R24  107.48  -0.0  0.400  -0.0  0.400
469 R24  93.49   0.0  0.400   0.0  0.400
493 R24  121.13  0.0  0.400   0.0  0.400
841 R24  105.58  0.0  0.400   0.0  0.400
853 R24  120.18  -0.0  0.400   0.0  0.400
865 R24  133.09  0.0  0.400  -0.0  0.400
-----
Factored Stress and Capacity:
-----
Node Pile Label   vu   f'c   Phi*vc   Critical Point X_Offset Y_Offset Status
-----
97 R24   10.48  3000.00  164.32  -1.85 -1.85 Safe
109 R24  12.38  3000.00  164.32  -0.00 -2.61 Safe
121 R24  14.08  3000.00  164.32  -0.00 -2.61 Safe
469 R24  12.25  3000.00  164.32  -2.61 -0.00 Safe
493 R24  15.87  3000.00  164.32  1.19  2.33 Safe
841 R24  13.84  3000.00  164.32  -2.61 -0.00 Safe
853 R24  15.75  3000.00  164.32  1.54 -2.12 Safe
865 R24  17.44  3000.00  164.32  2.12  1.54 Safe

```

Figure 12 – Two-Way Shear Results around Piles

3. Pile Reactions

The model results provide a detailed list of the pile reactions indicating the magnitude and direction of the resulting forces on each pile in the foundation model. Whether force is downward compression or upward net tension on the pile, the load combination producing the maximum reaction is denoted in the output results table.

```

B3 - REACTIONS:
=====
Units --> Force (kip), Moment (kip-ft)
Service Load Combination: 1.0D + 1.0W

```

Node	Soil	Spring	Pile	Restrains			Slaved Nodes		
	Fz	Fz	Fz	Fz	Mx	My	Fz	Mx	My
97	0.139	-	101.762	-	-	-	-	-	-
109	0.152	-	111.188	-	-	-	-	-	-
121	0.162	-	118.957	-	-	-	-	-	-
469	0.151	-	110.593	-	-	-	-	-	-
493	0.174	-	127.869	-	-	-	-	-	-
841	0.161	-	117.773	-	-	-	-	-	-
853	0.174	-	127.274	-	-	-	-	-	-
865	0.184	-	134.967	-	-	-	-	-	-

Sum of all forces and moments with respect to center of gravity (X, Y) = (7.50, 7.50) ft

Sum of Reactions	Fz	Mx	My
Soil	146.357	30.860	-33.142
Springs	-	-	-
Piles	950.383	288.641	-309.984
Restrains	-	-	-
Slaved Nodes	-	-	-
Total Reactions	1096.740	319.501	-343.126
Total Loads	-1096.740	-319.501	343.126

Figure 13 – Piles Service Reactions

```

B3 - REACTIONS:
=====
Units --> Force (kip), Moment (kip-ft)
Ultimate Load Combination: 0.9D + 1.0W

```

Node	Soil	Spring	Pile	Restrains			Slaved Nodes		
	Fz	Fz	Fz	Fz	Mx	My	Fz	Mx	My
97	0.109	-	79.964	-	-	-	-	-	-
109	0.129	-	94.439	-	-	-	-	-	-
121	0.147	-	107.475	-	-	-	-	-	-
469	0.127	-	93.488	-	-	-	-	-	-
493	0.165	-	121.128	-	-	-	-	-	-
841	0.144	-	105.581	-	-	-	-	-	-
853	0.164	-	120.177	-	-	-	-	-	-
865	0.182	-	133.092	-	-	-	-	-	-

Sum of all forces and moments with respect to center of gravity (X, Y) = (7.50, 7.50) ft

Sum of Reactions	Fz	Mx	My
Soil	131.721	49.376	-53.027
Springs	-	-	-
Piles	855.345	461.826	-495.975
Restrains	-	-	-
Slaved Nodes	-	-	-
Total Reactions	987.066	511.202	-549.002
Total Loads	-987.066	-511.202	549.002

Figure 14 – Piles Ultimate Reactions

Note: Positive and negative reaction values indicate compression and tension forces in piles, respectively.

4. Pile Cap Model Statistics

Since spMats is utilizing finite element analysis to model and design the foundation. It is useful to track the number of elements and nodes used in the model to optimize the model results (accuracy) and running time (processing stage). spMats provides model statistics to keep tracking the mesh sizing as a function of the number of nodes and elements.

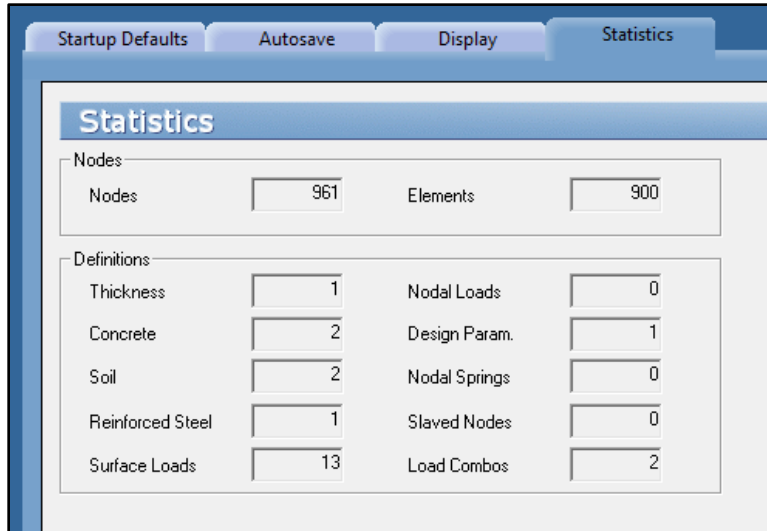


Figure 15 – Model Statistics

5. Column and Pile Design - spColumn

spMats provides the options to export columns and pile information from the foundation model to spColumn. Input (CTI) files are generated by spMats to include the section, materials, and the loads from the foundation model required by spColumn for strength design and investigation of piles and columns. Once the foundation model is completed and successfully executed, the following steps illustrate the design of a sample pile and column.

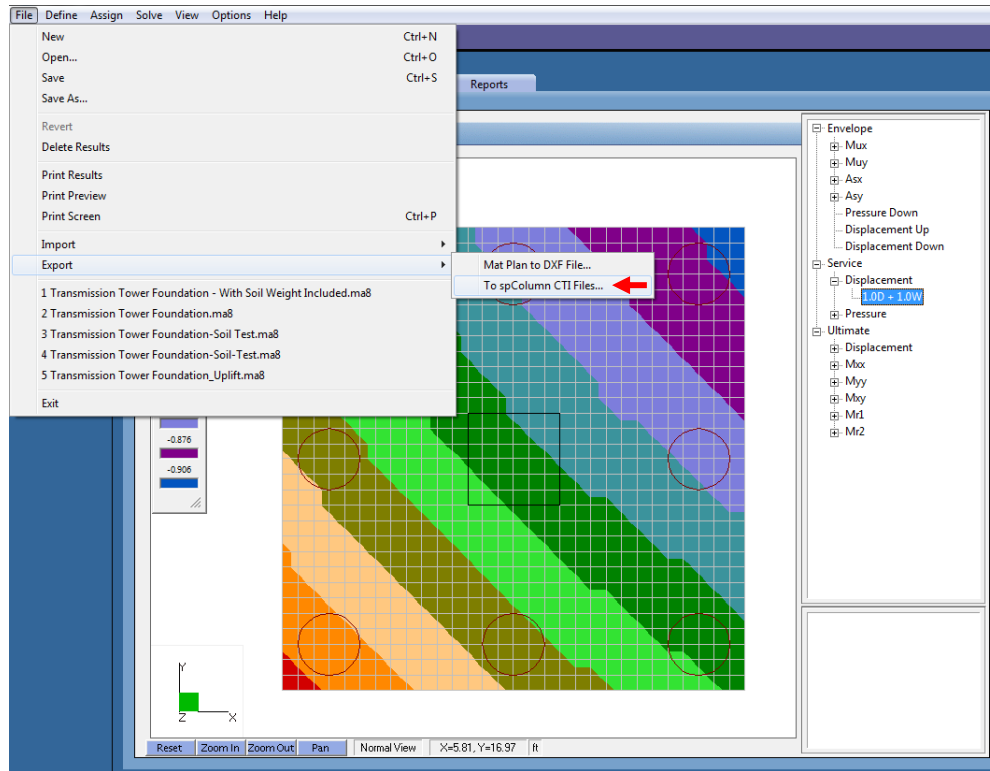


Figure 16 – Exporting CTI Files

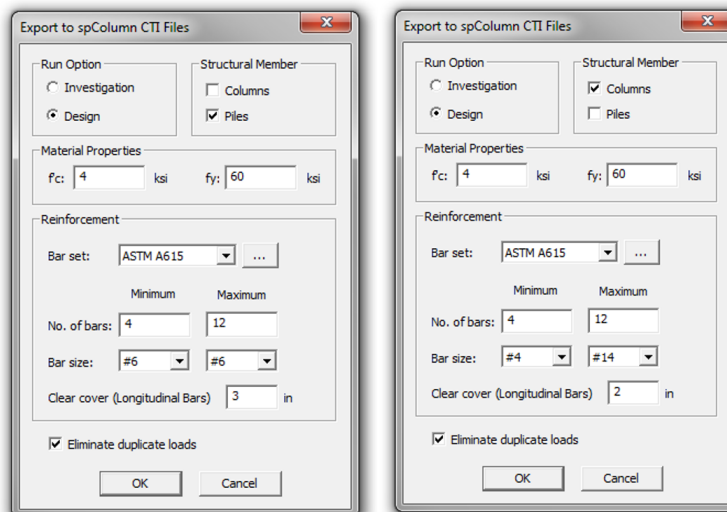


Figure 17 – Exporting CTI Files Dialog Box

After exporting spColumn input files, the pile and column design/investigation can proceed/modified to meet project specifications and criteria. In the following a sample pile and column design results are shown as an example.

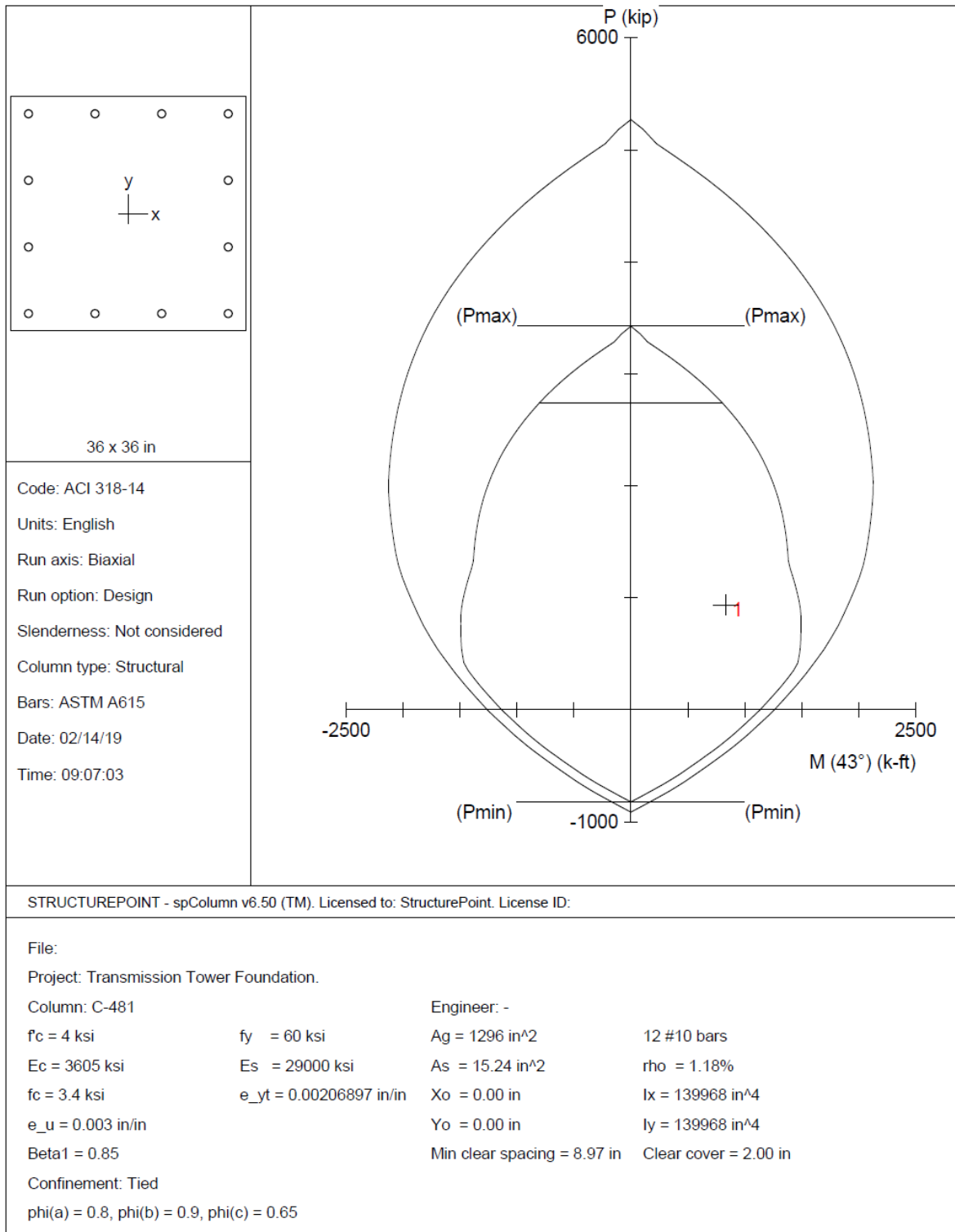


Figure 18 – Concrete Pier Interaction Diagram with Factored Load

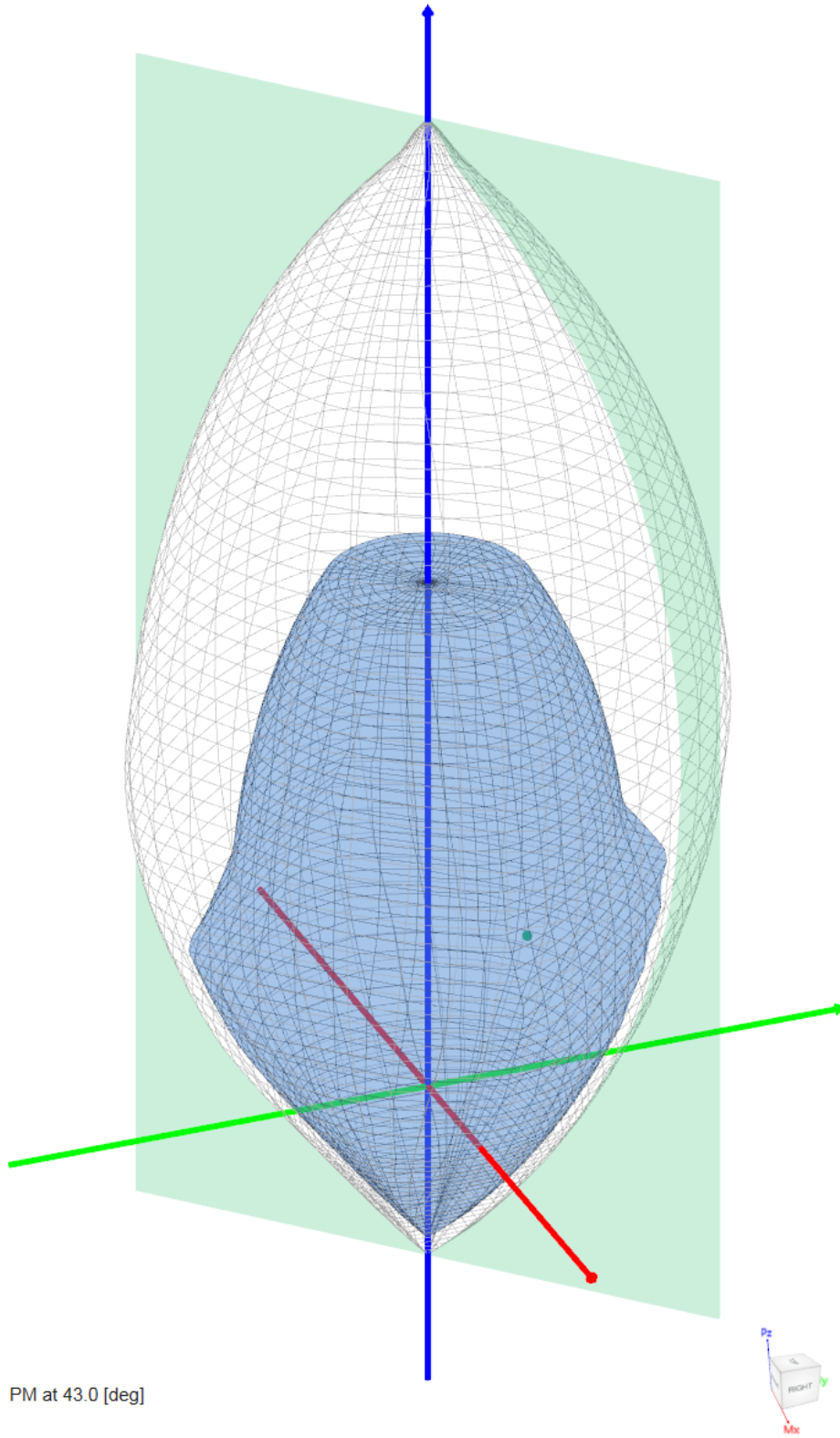


Figure 19 – Column 3D Failure Surfaces

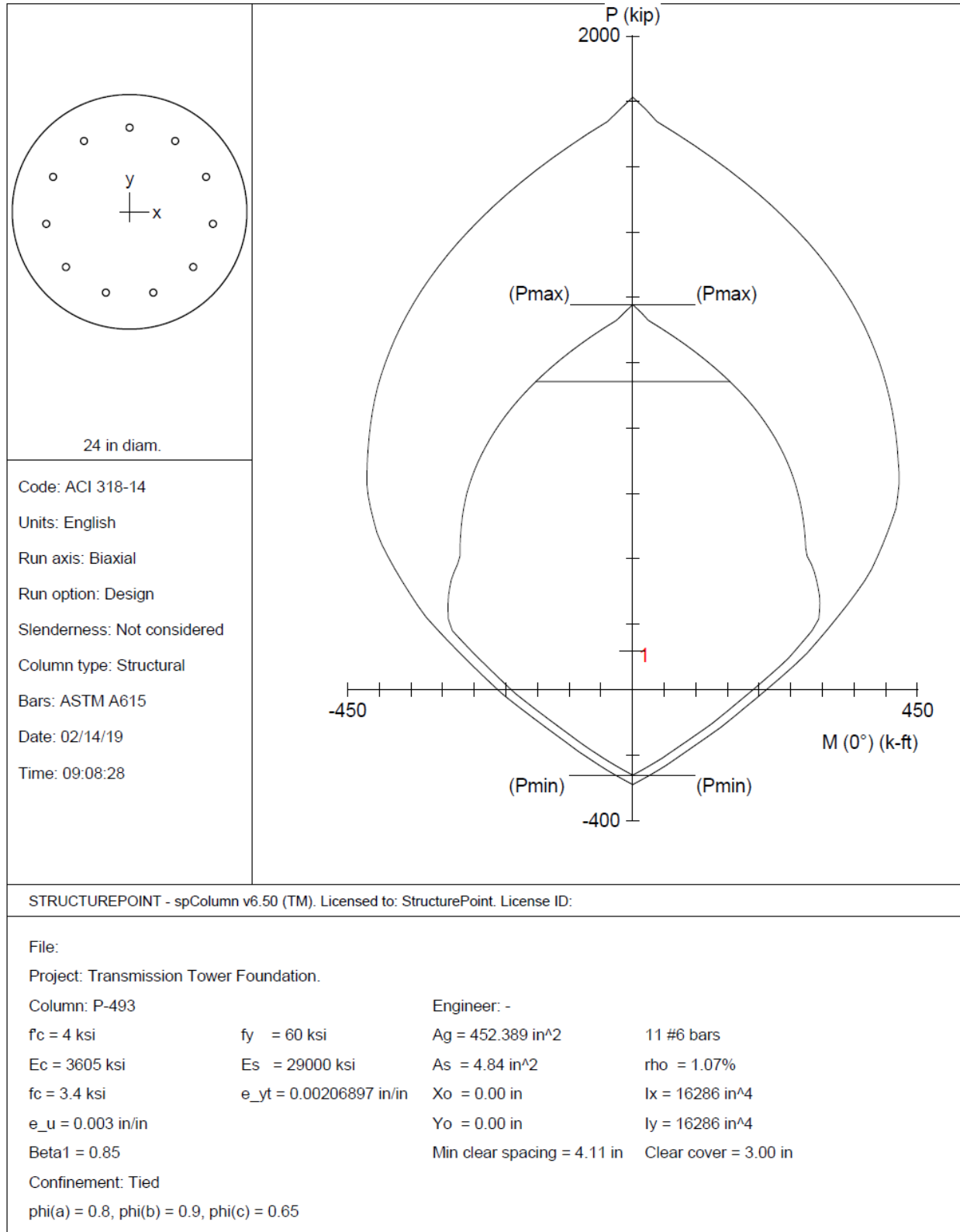


Figure 20 – Pile Interaction Diagram with Reaction Applied

6. 2D/3D Viewer

2D/3D Viewer is an advanced module of the [spColumn](#) program. It enables the user to view and analyze 2D interaction diagrams and contours along with 3D failure surfaces in a multi viewport environment.

2D/3D Viewer is accessed from within [spColumn](#). Once a successful run has been performed, you can open 2D/3D Viewer by selecting the **2D/3D Viewer** command from the **View** menu. Alternatively, 2D/3D Viewer can also be accessed by clicking the 2D/3D Viewer button in the program toolbar.

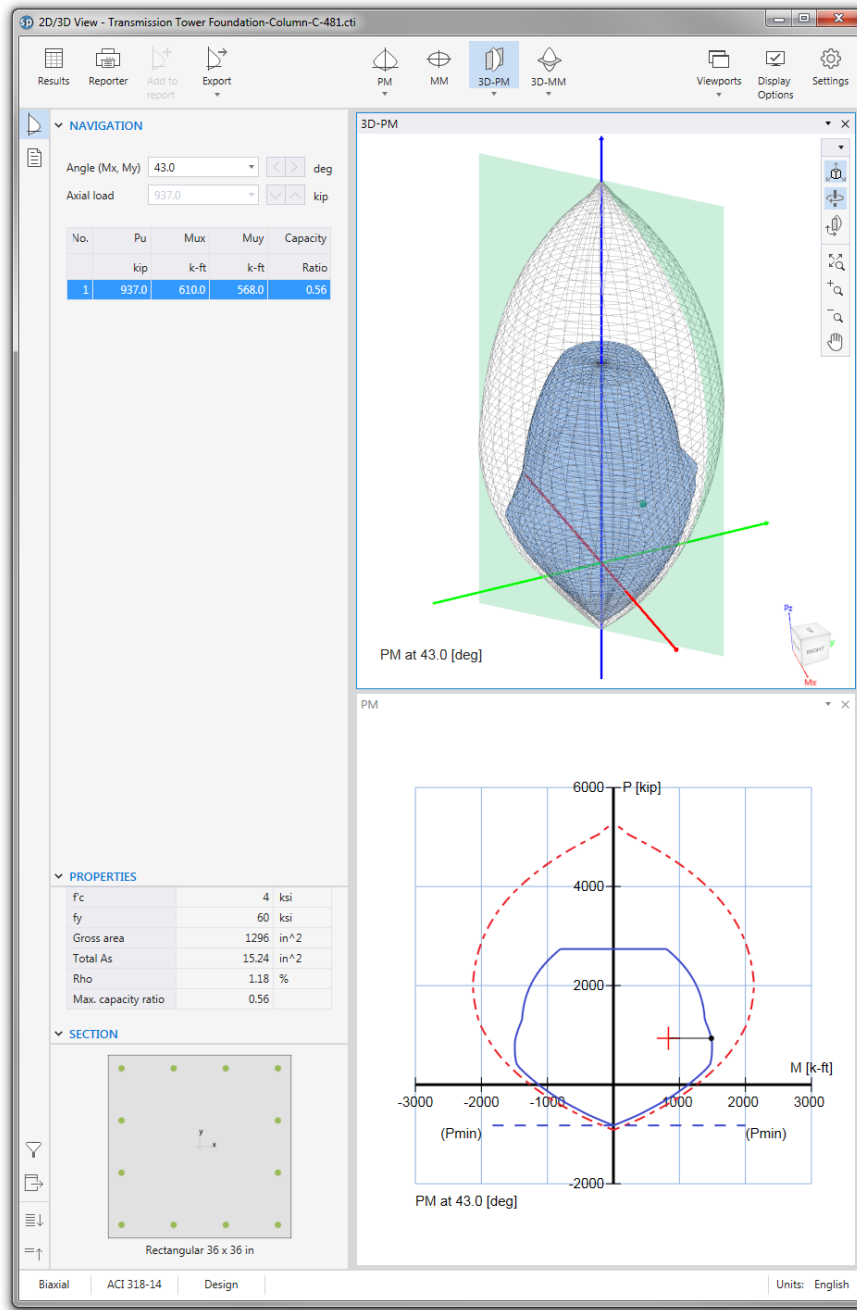


Figure 21 – 2D/3D View for Column

7. Tied vs. Spiral Confinement

The builder was provided two options for confinement to increase field and construction flexibility. The impact of spiral vs tied confinement is illustrated below.

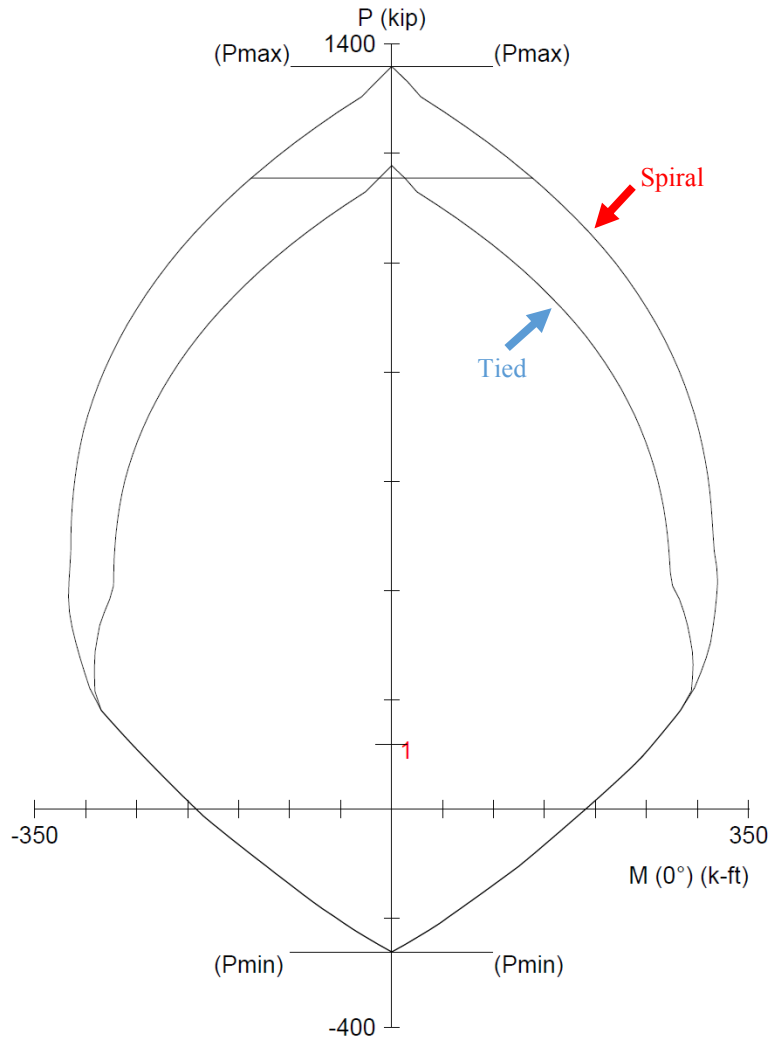


Figure 22 – Tied vs. Spiral Confinement